

# ME 321: Fluid Mechanics-I

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Lecture - 10 (05/07/2025)
Fluid Dynamics: Applications of Bernoulli Equation

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A U-tube acts as a water siphon. The bend in the tube is 1 m above the water surface; the tube outlet is 7 m below the water surface. The water issues from the bottom of the siphon as a free jet at atmospheric pressure. Determine (after listing the necessary assumptions) the speed of the free jet and the minimum absolute pressure of the water in the bend.

#### Solution:

**Assumptions:** (1) Neglect friction.

(2) Steady flow.

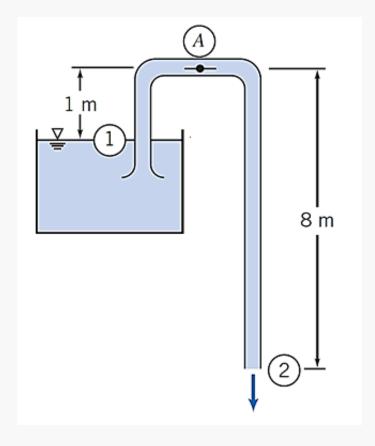
- (3) Incompressible flow. Irrotational flow
- (4) Flow along a streamline.
- (5) Reservoir is large compared with pipe.

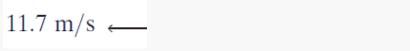
Apply the Bernoulli equation between points (1) and (2).

$$\frac{p_1}{\rho} + \frac{V_1^2}{2} + gz_1 = \frac{p_2}{\rho} + \frac{V_2^2}{2} + gz_2$$

Since area<sub>reservoir</sub>  $\gg$  area<sub>pipe</sub>, then  $V_1 \approx 0$ . Also  $p_1 = p_2 = p_{\text{atm}}$ , so

$$gz_1 = \frac{V_2^2}{2} + gz_2$$
 and  $V_2^2 = 2g(z_1 - z_2)$ 







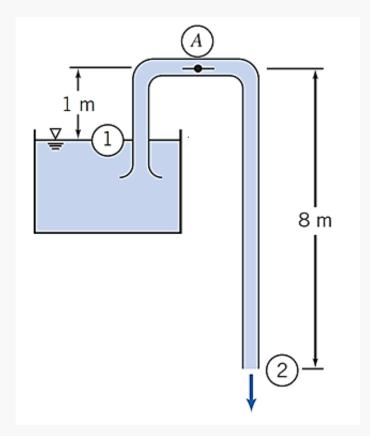
To determine the pressure at location (A), we write the Bernoulli equation between (1) and (A).

$$\frac{p_1}{\rho} + \frac{V_1^2}{2} + gz_1 = \frac{p_A}{\rho} + \frac{V_A^2}{2} + gz_A$$

Again  $V_1 \approx 0$  and from conservation of mass  $V_A = V_2$ . Hence

$$\frac{p_A}{\rho} = \frac{p_1}{\rho} + gz_1 - \frac{V_2^2}{2} - gz_A = \frac{p_1}{\rho} + g(z_1 - z_A) - \frac{V_2^2}{2}$$

$$p_A = 22.8 \text{ kPa (abs) or } -78.5 \text{ kPa (gage)} \leftarrow$$





# Real flow system



Modification of Bernoulli equation is a must for real flow systems:

Real flow systems must account for loss of energy, which is frequently known as head loss.

- 1) Major loss (due to viscous effect /fluid friction /viscosity)
- 2) Minor loss / local losses (due to different pipe fittings, etc.)

Details in ME 323

**Modified** Bernoulli relation comes as:

$$\frac{p_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{p_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + \frac{1}{2g} + \frac{1}{2g}$$

- (1) is the upstream point and
- (2) is the downstream point

$$h_L$$
 = head loss

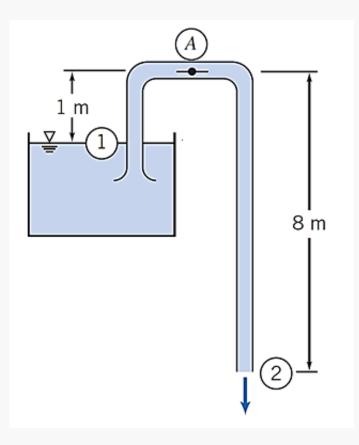
$$h_L = \sum f \frac{L}{D} \frac{v^2}{2g} + \sum k \frac{v^2}{2g}$$





A U-tube acts as a water siphon. The bend in the tube is 1 m above the water surface; the tube outlet is 7 m below the water surface. The water issues from the bottom of the siphon as a free jet at atmospheric pressure. Determine (after listing the necessary assumptions) the speed of the free jet and the minimum absolute pressure of the water in the bend if the head loss count is

$$h_L \approx 2.3 \; \frac{V^2}{2g}$$







The liquid in the figure below is kerosene (SG = 0.8). Estimate the flow rate from the tank for

- (a) No losses and
- (b) Pipe losses  $h_L \approx 4.5 \frac{V^2}{2g}$

#### Solution:

(a) 
$$\frac{p_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{p_2}{\gamma} + \frac{V_2^2}{2g} + z_2$$

$$\Rightarrow \frac{140 \times 10^3}{\gamma} + \frac{0^2}{2g} + 1.5 = \frac{101.3 \times 10^3}{\gamma} + \frac{V_2^2}{2g} + 0$$

$$\Rightarrow V_2 = (\equiv V)$$

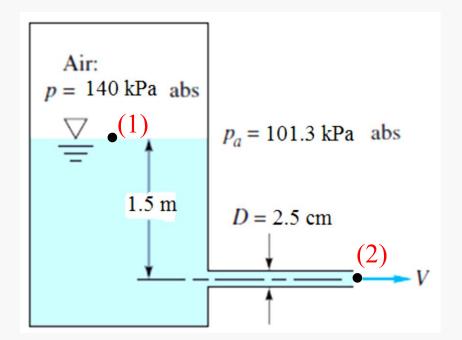
$$\therefore Q = AV = ?$$

(b) 
$$\frac{p_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{p_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_L$$

$$\Rightarrow \frac{140 \times 10^3}{\gamma} + \frac{0^2}{2g} + 1.5 = \frac{101.3 \times 10^3}{\gamma} + \frac{V_2^2}{2g} + 0 + 4.5 \frac{V_2^2}{2g}$$

$$\Rightarrow V_2 = (\equiv V)$$

$$\therefore Q = AV = ?$$





# Flow system with turbomachinery



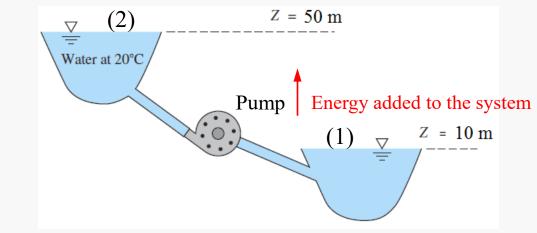
Modified Bernoulli equation i.e. the **energy equation** in a **flow system with pump**:

No head loss: 
$$\frac{p_1}{\gamma} + \frac{V_1^2}{2g} + z_1 + h_P = \frac{p_2}{\gamma} + \frac{V_2^2}{2g} + z_2$$

With head loss:  $\frac{p_1}{\gamma} + \frac{V_1^2}{2\rho} + z_1 + h_P = \frac{p_2}{\gamma} + \frac{V_2^2}{2\rho} + z_2 + h_L$ 

 $h_P$  = head (energy) added to the system

$$P_{pump} = \gamma Q h_P$$
 (pump hydraulic power)



Pump:

Input: Electrical power (in general)

Output: hydraulic power

$$\eta = \frac{P_{out}}{P_{in}} = \frac{\gamma Q h_P}{P_{in} \text{ (elect. power)}}$$

$$h_L$$
 = head loss (major/minor) to be added at downstream





# Flow system with turbomachinery

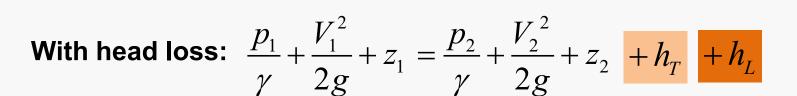


Modified Bernoulli equation i.e. the **energy equation** in a **flow system with turbine**:

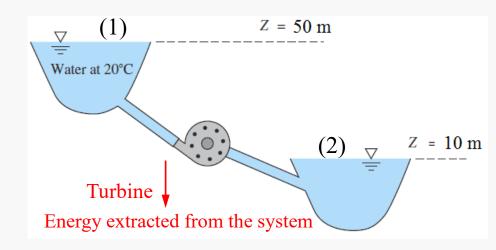
No head loss: 
$$\frac{p_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{p_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_T$$

 $h_T$  = head (energy) extracted from the system

$$P_{turbine} = \gamma Q h_T$$
 (turbine hydraulic power)



 $h_L$  = head loss (major/minor) to be added at downstream



Turbine:

Input: hydraulic/mechanical power

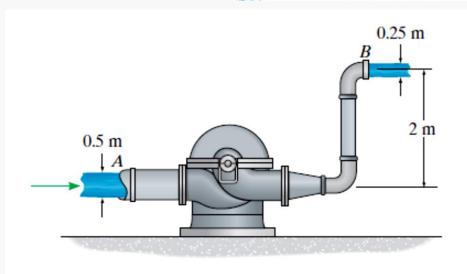
Output: Electrical power

$$\eta = \frac{P_{out}}{P_{in}} = \frac{P_{in} \text{ (elect. power)}}{\gamma Q h_T}$$



The electrical power input to the pump is 10 kW. If the pump has an efficiency of 80%, and the increase in pressure from **A** to **B** is 100 kPa, determine the volumetric flow rate of water through the pump in cases of

- (i) No head loss between A to B
- (ii) Head loss between A to B is 1.25 m.



#### Solution:

(i) No head loss between A to B:

Bernoulli equation between points A and B for this case is-

$$\frac{p_A}{\gamma} + \frac{V_A^2}{2g} + z_A + h_p = \frac{p_B}{\gamma} + \frac{V_B^2}{2g} + z_B$$
 (i)

;  $h_p$  is the head developed by the pump

From continuity equation:

$$Q = v_A A_A = v_B A_B \qquad \text{(unknown)}$$

$$\Rightarrow Q = v_A \left(\frac{\pi}{4} d_A^2\right) = v_B \left(\frac{\pi}{4} d_B^2\right)$$

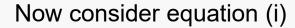
$$\Rightarrow Q = v_A \left(\frac{\pi}{4} 0.5^2\right) = v_B \left(\frac{\pi}{4} 0.25^2\right)$$

$$\Rightarrow V_A = 5.09Q \qquad \& \quad v_B = 20.37Q$$



For the pump

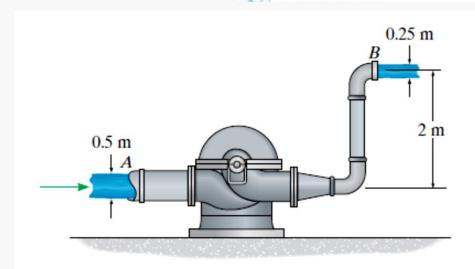
$$\eta = \frac{P_{out}}{P_{in}} \left( \frac{\text{Hydraulic power output}}{\text{Electrical power input}} \right) 
\Rightarrow 0.8 = \frac{P_{out}}{10 \times 10^3} 
\Rightarrow P_{out} = 0.8 \times 10 \times 10^3 
\Rightarrow \gamma Q h_P = 0.8 \times 10 \times 10^3 
\Rightarrow h_P = \frac{0.8 \times 10 \times 10^3}{\gamma Q} \qquad \Rightarrow h_P = \frac{0.8155}{Q}$$



$$\frac{p_A}{\gamma} + \frac{V_A^2}{2g} + z_A + h_P = \frac{p_B}{\gamma} + \frac{V_B^2}{2g} + z_B \qquad (i)$$

$$\Rightarrow \frac{V_A^2}{2g} + 0 + h_P = \frac{p_B - p_A}{\gamma} + \frac{V_B^2}{2g} + 2$$

$$\Rightarrow \frac{(5.09Q)^2}{2g} + 0 + \frac{0.8155}{Q} = \frac{100 \times 10^3}{(1000 \times 9.81)} + \frac{(20.37Q)^2}{2g} + 2$$



$$\Rightarrow \frac{0.8155}{Q} = 12.19 + 19.83Q^2$$

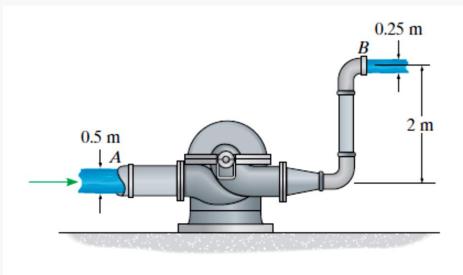




On solving the last equation to get the flow rate, Q: (through numerical solution)

$$\Rightarrow \frac{0.8155}{Q} = 12.19 + 19.83Q^{2}$$

$$\Rightarrow Q \approx 0.0664 \text{ m}^{3}/\text{s} \quad (\equiv 239\text{m}^{3}/\text{hr}, 66.41/\text{s})$$
 Ans. (i)



#### (ii) Head loss between A to B is 1.25 m:

Bernoulli equation between points A and B for this case is-

$$\frac{p_A}{\gamma} + \frac{{V_A}^2}{2g} + z_A + h_P = \frac{p_B}{\gamma} + \frac{{V_B}^2}{2g} + z_B + h_L$$
 (ii)

;  $h_p$  is the head developed by the pump  $h_L$  is the head loss from points A to B

$$\Rightarrow \frac{V_A^2}{2g} + 0 + h_P = \frac{p_B - p_A}{\gamma} + \frac{V_B^2}{2g} + 2 + 1.25$$

$$\Rightarrow \frac{(5.09Q)^2}{2g} + 0 + \frac{0.8155}{Q} = \frac{100 \times 10^3}{(1000 \times 9.81)} + \frac{(20.37Q)^2}{2g} + 3.25$$

$$\Rightarrow \frac{0.8155}{Q} = 13.44 + 19.83Q^2$$

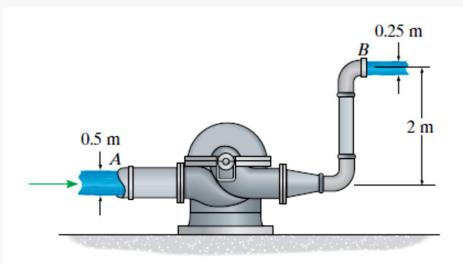




On solving the last equation to get the flow rate, Q: (through numerical solution)

$$\Rightarrow \frac{0.8155}{Q} = 13.44 + 19.83Q^{2}$$

$$\Rightarrow Q \approx 0.0604 \text{ m}^{3}/\text{s} \quad (\equiv 218\text{m}^{3}/\text{hr}, 60.41/\text{s})$$
 Ans. (ii)



Volumetric flow rate will be reduced in case of head loss due to fluid friction (major loss) and pipe fittings (minor loss).

Head losses will be covered in detail in ME 323 (L3 T2)



Find the power requirement of the 85%-efficient pump shown in Fig. if the loss coefficient up to A is 3.2, and from B to C, K=1.5. Neglect the losses through the exit nozzle.

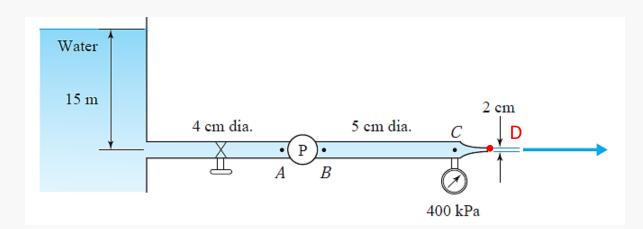
Also, calculate  $p_A$  and  $p_B$ .

#### Solution:

$$Q_C = Q_D$$

$$\frac{\pi}{4} 0.05^2 \,\mathsf{V_C} = \frac{\pi}{4} 0.02^2 \,\mathsf{V_D}$$

$$\therefore V_C = 0.16 \,VD$$



$$h_L = K \frac{V^2}{2g}$$

Bernoulli equation between points C and D (across the nozzle) -

$$\frac{p_C}{\gamma} + \frac{{V_C}^2}{2g} + z_C = \frac{p_D}{\gamma} + \frac{{V_D}^2}{2g} + z_D + h_{LC-D}$$

$$\frac{400 \times 10^3}{9810} + \frac{(0.16V_D)^2}{2g} + 0 = 0 + \frac{{V_D}^2}{2g} + 0 + 0$$

$$\therefore VD = 28.6 \, m/s$$

$$\therefore VC = 4.6 \, m/s$$

;  $h_{LC-D} = 0$  (no loss through the nozzle)





Considering points B and C -

$$Q_B = Q_C$$

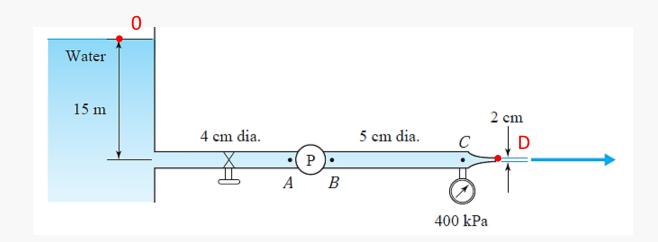
$$\therefore VB = VC = 4.6 \, m/s$$

Considering points A and C -

$$Q_A = Q_C$$

$$\frac{\pi}{4} 0.04^2 \, V_A = \frac{\pi}{4} 0.05^2 (4.6)$$

$$\therefore VA = 7.2 \, m/s$$



Bernoulli equation between points 0 and D (surface to exit) -

$$\frac{p_0}{\gamma} + \frac{{V_0}^2}{2g} + z_0 + hp = \frac{p_D}{\gamma} + \frac{{V_D}^2}{2g} + z_D + h_{L 0 - D}$$

$$0 + 0 + 15 + hp = 0 + \frac{28.6^2}{2g} + 0 + 3.2 + \frac{7.2^2}{2g} + 1.5 + \frac{4.6^2}{2g}$$

$$; h_{L 0-D} = h_{L 0-A} + h_{L B-D} = KA \frac{V_A^2}{2g} + K_B \frac{V_B^2}{2g}$$

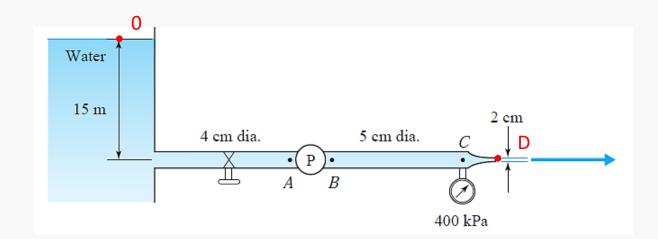


: hp = 36.8 m



Pump requirement to run the pump

$$P_{elect.} = \frac{\gamma QhP}{\eta}$$
=\frac{(9810)(\frac{\pi}{4}\times 0.02^2\times 28.6)(36.8)}{0.85}
= 3.82 \text{ kW (Ans.)}



Bernoulli equation between points 0 and A (surface to A) -

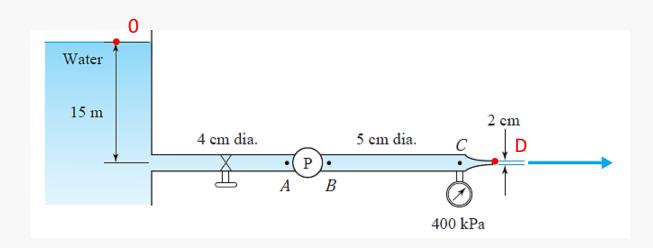
$$\frac{p_0}{\gamma} + \frac{{V_0}^2}{2g} + z_0 = \frac{p_A}{\gamma} + \frac{{V_A}^2}{2g} + z_A + h_{L \, 0-A}$$

$$0 + 0 + 15 = \frac{p_A}{\gamma} + \frac{7.2^2}{2g} + 0 + 3.2 \frac{7.2^2}{2g}$$

$$\therefore pA = 38.3 \ kPa \ (Ans.)$$







Bernoulli equation between points 0 and B (surface to B) -

$$\frac{p_0}{\gamma} + \frac{{V_0}^2}{2g} + z_0 + hp = \frac{p_B}{\gamma} + \frac{{V_B}^2}{2g} + z_B + h_{L \, 0-B}$$

$$0 + 0 + 15 + 36.8 = \frac{p_B}{\gamma} + \frac{4.6^2}{2g} + 0 + 3.2 \frac{7.2^2}{2g}$$

$$\therefore pB = 414.6 \ kPa \ (Ans.)$$

$$; h_{L \ 0-B} = h_{L \ 0-A} + h_{L \ A-B} = KA \frac{V_A^2}{2g} + 0$$

